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Decomposition of Nitrous Oxide over Cu/TiO₂ Catalysts: The Effect of Cu Loading, TiO₂ Structure, and Reaction Conditions

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ABSTRACT

Decomposition of nitrous oxide (N₂O) over titania (TiO₂) supported copper (Cu) catalyst was investigated with the existence of oxygen and water vapor. The catalytic activity of TiO₂ was promoted by copper loading. It was found that there are optimum levels of copper loading on TiO₂, and these values are correlated to the specific surface area of TiO₂ support being used. The relationship between the catalytic activity for decomposition of N₂O and the crystal structure of TiO₂ was also investigated. The result revealed that Cu/TiO₂ catalysts with the rutile structure has a higher activity toward N₂O decomposition than those with the anatase structure. In this research, Cu(5wt%)/TiO₂ prepared from TiO₂ JRC-TIO-4 (reference catalyst provided by Catalysis Society of Japan) which was mainly constituted of rutile showed the highest activity for N₂O decomposition and it could decompose N₂O completely at 650°C. The catalytic activity was inhibited by the existence of oxygen. However, there was no influence of water vapor to the catalytic activity of Cu/TiO₂ for N₂O decomposition.

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1. INTRODUCTION

Nitrous oxide (N_2O) is one of the powerful greenhouse gases with a global warming potential per molecule of about 300 times higher than that of carbon dioxide (CO_2) . N_2O is also identified as a contributor to the destruction of ozone layer in the stratosphere. Therefore, from the environmental point of view, it is important to investigate the decomposition of N₂O to minimize its adverse effect on the environment. A considerable number of studies have been conducted on the catalytic decomposition and the selective catalytic reduction of N_2O (Haber et al., 2004; Dandekar & Vannice, 1999; Lin et al., 1996; Triawan et al., 2018; Tanaka et al., 2000; Chaki et al., 2003; Pophal et al., 1998; Yan et al., 2003; Sunnardianto et al., 2019).

Selective catalytic reduction of NO to N2 over TiO2-supported metal catalysts in the presence of hydrocarbon had been studied by Mitadera and Hinode (2002), and the results showed that TiO₂supported metal catalysts had good activity for NO reduction (Mitadera & Hinode, 2002). The mechanism of NO reduction to N₂ involves the production of N₂O which occurs at low temperature region. From this result, it could be interpreted that N₂O produced from NO reduction was completely decomposed at high temperature region. Therefore, it was assumed that TiO₂-supported metal catalysts would also show a good activity for N₂O decomposition.

Furthermore, TiO₂ as a support also possesses advantages such as high tolerance to water vapor, which is an important property for N₂O decomposition catalyst in practical use, where oxygen and water vapor often exist in the N₂O containing stream. Therefore, it is desirable to investigate the activity of TiO₂supported metal catalysts for decomposition of N₂O. In this study, the direct decomposition of N₂O to N₂ by various Cu/TiO₂ catalysts was investigated to understand the influences of Cu loading, TiO₂ structure, as well as oxygen and water vapor on the catalytic activity of the catalyst.

2. METHODOLOGY

2.1. Catalyst Preparation

In this research, Cu/TiO₂ catalyst was prepared by impregnation method. Vari-

ous kinds of TiO₂ (JRC-TIO-1, 2, 4, and 6; reference catalyst provided by Catalysis Society of Japan) were used as supports. The specific surface area of JRC-TIO-1, 2, 4, and 6 are 82.0 m²/g, 15.9 m²/g, 52.9 m²/g, and 73.0 m²/g, respectively.

Parent TiO₂ was stirred in a aqueous solution of Cu(NO₃)₂ • 3H₂O (99.9%, Wako Co.) at room temperature for one day. Afterwards, the impregnated catalysts were dried up at approximately 60°C for one day, followed by calcination at 600°C for 5 hours under air flow. In order to reduce the pressure drop in the catalytic activity study, catalysts were pelletized, crushed and sieved to between 0.71 mm to 1.00 mm. The catalyst samples were expressed as: Cu(x wt%)/TiO₂ y, where x means Cu loading level, and y represents reference support number (e.g. Cu(1wt%)/TiO₂ (1) means JRC-TIO-1 loading by 1 wt% of Cu).

2.2. Experimental procedure and characterizations

The catalytic reaction was carried out in a fixed-bed flow reactor under atmospheric pressure. A 1.0 g sample was packed in a quartz tube with 6 mm inner diameter. The reactant gas was prepared by mixing N₂O, O₂, and He gas. The mixed gas of 1,000 ppm of N₂O and 10% of O₂ (He as balance gas) was fed to the catalyst at a flow rate of 5.0-6.0 ml/s, which corresponded to space velocity of 16,000 h-1. Water vapor was introduced to the reactor by bubbling system with concentration of approximately 5 vol%.

Gas chromatograph (GC323w; GL Science Co., with Porapak N, Porapak Q and Molecular Sieve 13X column) was used to analyze the concentration of N_2O , N_2 and O_2 after leaving the catalyst system. Characterization of catalyst was performed by X-ray Diffraction (XRD) Method (MultiFlex; Rigaku) and N_2 Adsorption-Desorption Method (SA3100; COULTER).

3. RESULT AND DISCUSSION

3.1. The decomposition of N₂O over Cu/TiO₂

The catalytic activities of Cu/TiO₂ catalysts with different TiO₂ support (JRC-TIO-1, 2, 4, and 6) for the decomposition of N₂O were investigated. The experimental results without the presence of water vapor are shown in **Figures 1** to **4**.

Figure 1 shows the effect of Cu loading level of Cu/TiO₂(1) on the decomposition of N₂O to N₂. The catalyst with Cu loading of 10wt% showed the highest catalytic activity, and the decomposition began at the temperature of 400°C. Complete conversion of N₂O to N₂ was obtained in the temperature range of 650 to 700°C.

Figure 2 shows the effect of Cu loading level of Cu/TiO₂(2) on the decomposition of N₂O to N₂. In this case, the catalyst with Cu loading of 5wt% showed the highest catalytic activity. However, the difference of catalytic activity with respect to the change of Cu loading level was not significant.



Figure 1. Effect of Cu loading level of Cu/TiO₂ \bigcirc on the decomposition of N₂O to N₂



Figure 2. Effect of Cu loading level of Cu/TiO₂ on the decomposition of N₂O to N₂.

Figure 3 shows the effect of Cu loading level of Cu/TiO₂(4) on the decomposition of N₂O to N₂. It can be seen from Figure 3 that JRC-TIO-4 decomposed only approximately 35% of N₂O to N₂ at 700°C. Supporting copper on JRC-TIO-4 resulted in the improvement of catalytic activity. In this case, the catalyst with Cu loading level of 5wt% showed the highest catalytic activity.



Figure 3. Effect of Cu loading level of Cu/TiO₂(4) on the decomposition of N₂O to N₂

Figure 4 shows the effect of Cu loading level of Cu/TiO₂⁽⁶⁾ on the decomposition of N₂O to N₂. In this case, the catalysts with 5wt% and 10wt% Cu loading levels showed almost the same catalytic activity for the decomposition.</sup>



Figure 4. Effect of Cu loading level of Cu/TiO₂⑥ on the decomposition of N₂O to N₂.

3.2. The relationship between the optimum Cu loading level and specific surface area of TiO₂

In Section 3.1, it was observed that the optimum Cu loading levels of Cu/TiO₂ for each TiO₂ support were as followed: JRC-TIO-1; 10wt%, JRC-TIO-2; 1wt%, JRC-TIO-4; 5wt%, and JRC-TIO-6; 5wt%. This difference of the optimum Cu loading level was considered to be correlated with the difference of the specific surface area of each TiO₂ support.

The X-ray Diffraction (XRD) analysis showed CuO was identified as the copper species on TiO_2 . Therefore, the projected

area of one molecule of CuO on the surface of TiO₂ can be calculated using the radius of Cu²⁺ ion and O²⁻ ion and the bonding distance of Cu-O molecule. The radius of Cu²⁺ ion and O²⁻ ion are 0.69 Å and 1.40 Å respectively, and the bonding distance of Cu-O is 1.95 Å. From these data, the projected area (S) of one molecule of CuO on the surface of TiO₂ can be geometrically calculated by using equation (1) to approximately 7.59 Å².

$$S = \int_{-1.40}^{1.355} \sqrt{1.40^2 - x^2} \, dx + \int_{1.355}^{2.64} \sqrt{0.69^2 - (x - 1.95)^2} \, dx$$
 (1)

during impregnation, However, Cu(NO₃)₂ was dispersed rather than CuO and loaded on the surface of TiO2. Therefore the projected area of Cu(NO₃)₂ on TiO₂ surface was also calculated. The necessary amount of CuO or Cu(NO₃)₂ molecule to make the monolayer on the surface of TiO₂ can be calculated by assuming the TiO₂ surface was uniform and the molecules of CuO or Cu(NO₃)₂ composed the first monolayer on the surface of TiO₂. Table 1 shows the relationship between the specific surface area of TiO₂ and the optimum Cu loading level of Cu/TiO₂ from the catalytic activity experiments and from the geometrical calculation of CuO and $Cu(NO_3)_2$ projected area.

Support	Specific sur- face area [m²/g]	Optimum Cu loading level [wt%]		
		Experimental data	Geometrical cal- culation of CuO	Geometrical calcula- tion of Cu(NO ₃) ₂
JRC-TiO-1	82.0	10	11.4	2.25
JRC-TIO-2	15.9	1	2.21	0.436
JRC-TIO-4	52.9	5	7.35	1.45
JRC-TIO-6	73.0	5	10.1	2.00

Table 1. Relationship between the specific surface area of TiO_2 and ideal Cu loading level for the decomposition of N_2O

The results from **Table 1** indicated that the optimum Cu loading level of Cu/TiO₂ obtained by the catalytic activity experiments showed a good correlation with the calculated value from the projected area of CuO. This finding suggested that when the TiO₂ surface was completely covered with CuO, the catalytic activity for the decomposition of N₂O reached maximum. If the amount of CuO loading exceeded the optimum loading, the catalytic activity remained the same or declined because of sintering of copper.

3.3. The relationship between crystal structure of TiO₂ and catalytic activity

Figure 5 shows the comparison of the catalytic activities of catalyst prepared from JRC-TIO-1, 2, 4, and 6. The Cu loading level for each sample was selected from loading level of the sample with the best result presented in section 3.1.

The specific surface area of JRC-TIO-2 was $15.9m^2/g$, and this value was evidently smaller than other samples. Optimum Cu loading level of Cu/TiO₂ prepared from JRC-TIO-2 was 1wt% which was also lower than other samples. This low loading level was considered as the cause of the low activity of Cu(1wt%)/TiO₂2.

The $Cu(5wt\%)/TiO_2$ and Cu(5wt%)/TiO₂6 showed higher catalytic activity than Cu(10wt%)/TiO₂(1), even though the optimum Cu loading levels of Cu/TiO₂ prepared from JRC-TIO-4 and JRC-TIO-6 were lower than that prepared from JRC-TIO-1. This result can be explained using the results of XRD analysis (Figure 6). The crystal structure of JRC-TIO-1 and JRC-TIO-2 was anatase and remained as anatase after the preparation of Cu/TiO₂. The crystal structure of JRC-TIO-6 was rutile, and it remained rutile structure after the preparation of Cu/TiO₂. Moreover, the main crystal structure of JRC-TIO-4 was anatase, and it changed to rutile after the

preparation of Cu/TiO₂. Therefore, the crystal structure of Cu(5wt%)/TiO24 and Cu(5wt%)/TiO₂6 was rutile, and the crystal structure of Cu(10wt%)/TiO₂1 and Cu(1wt%)/TiO₂2 was anatase.



Figure 5. The decomposition of N_2O to N_2 over Cu/TiO₂ prepared from each TiO₂





In **Figure 5**, $Cu(5wt\%)/TiO_2$ and $Cu(5wt\%)/TiO_2$ (rutile) exhibited higher catalytic activity for N₂O decomposition than $Cu(10wt\%)/TiO_2$ and $Cu(1wt\%)/TiO_2$ (anatase). This result suggested that the crystalline structure of

the support contributed to the catalytic activity of samples, and rutile is considered to be more effective than anatase for the decomposition of N_2O .

3.4. The influence of oxygen and water vapor on the N₂O decomposition to N₂

Figure 7 shows the influence of oxygen and water vapor on the decomposition of N₂O to N₂ over Cu(5wt%)/TiO₂($\frac{1}{4}$). In the absence of oxygen and water vapor, the decomposition of N₂O to N₂ over Cu(5wt%)/TiO₂($\frac{1}{4}$) began from the temperature of 400°C, and the conversion of N₂O to N₂ reached 100% at the temperature of 550°C. However, in the presence of oxygen, N₂O decomposition shifted to higher temperature. The temperature for 100% decomposition of N₂O to N₂ was higher than non-existent case.



Figure 7. Influence of oxygen and water vapor on the catalytic activity of Cu/TiO₂ for the decomposition of N_2O

 N_2O+O_2 system and $N_2O+O_2+H_2O$ system in **Figure 7** showed no difference of the catalytic activity for N_2O decomposition. Previous research reported that the catalytic activity for the decomposition of

 N_2O increased because of the existence of water vapor. However, our result in **Figure 7** showed that no difference of the catalytic activity for N_2O decomposition in N_2O+O_2 system and $N_2O+O_2+H_2O$ system. This indicates that the existence of water vapor does not influence this catalytic system, and the catalyst could be used in the water treatment process.

4. CONCLUSION

The decomposition of N₂O over various TiO₂-supported copper catalysts was investigated. Cu/TiO₂ catalyst exhibits catalytic activity for the decomposition of N₂O to N₂. Optimum Cu loading level is related to the specific surface area of TiO₂ support being used. The optimum Cu loading level increases with the specific surface area of TiO₂ support. Furthermore, when the TiO₂ surface is covered with CuO completely, the catalytic activity for the decomposition of N₂O reaches maximum value. On the basis of catalytic activity towards the decomposition of N₂O and XRD pattern of Cu/TiO₂ prepared from each TiO₂, rutile is considered to be more effective than anatase for the decomposition of N₂O. Therefore, $Cu(5wt\%)/TiO_2$ and $Cu(5wt\%)/TiO_2$ that constitute of rutile has the highest catalytic activity for the decomposition of N_2O to N_2 .

The catalytic activity for N_2O decomposition decreases in the existence of oxygen. However, the catalytic activity of Cu/TiO₂ for the decomposition of N_2O is not affected by water vapor. This water vapor tolerance of Cu/TiO₂ catalyst for the decomposition of N_2O is an advantage in the practical use.

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